

Phase Equilibrium in the System Ln-Mn-O at 1100°C

IX. Ln = Er and Tm

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Phase equilibrium was established in a Ln-Mn-O (Ln = Er and Tm) system at 1100 °C with the oxygen partial pressure ranging from $-\log (P_{O_2}/\text{atm}) = 0$ to 12.00, and phase diagrams for the corresponding $\text{Ln}_2\text{O}_3\text{-MnO-MnO}_2$ system at 1100°C were constructed. Stable Er_2O_3 , MnO, Mn_3O_4 , and ErMnO_3 phases were found in the Er-Mn-O system, and stable Tm_2O_3 , MnO, Mn_3O_4 , and TmMnO_3 phases were found in the Tm-Mn-O system.

LnMn_2O_5 , $\text{Ln}_2\text{Mn}_2\text{O}_7$, Ln_2MnO_4 , Mn_2O_3 , and MnO_2 were not found in either system.

Nonstoichiometric ranges were found in both LnMnO_3 phases, with the composition of LnMnO_3 represented as functions of $\log (P_{O_2}/\text{atm})$, $N_{\text{O}}/N_{\text{ErMnO}_3} = 2.68 \times 10^{-3} (\log P_{O_2}) - 0.008$ and $N_{\text{O}}/N_{\text{TmMnO}_3} = 2.53 \times 10^{-3} \log (P_{O_2}) - 0.005$

The activities of the components in a solid solution were calculated from the both equations.

The lattice constants of ErMnO_3 and TmMnO_3 quenched in air were determined.

The standard Gibbs energy changes of the reaction, $1/2 \text{Ln}_2\text{O}_3 + \text{MnO} + 1/4 \text{O}_2 = \text{LnMnO}_3$, appearing in the phase diagrams were also calculated. The relationship between the tolerance factors (t) of ErMnO_3 , TmMnO_3 and ΔG^0 values of the reaction, $1/2 \text{Ln}_2\text{O}_3 + \text{MnO} + 1/4 \text{O}_2 = \text{LnMnO}_3$, was shown graphically, together with other previous LnMnO_3 values. The two present ΔG^0 values were well-fitted to the general equation for hexagonal LnMnO_3 , $\Delta G^0 (\text{hexa}) = -6.426 \times 10^2 t + 5.406 \times 10^2$, which was previously obtained.

Key words: Phase equilibrium; Thermogravimetry; Erbium-manganese oxide; Thulium manganese oxide; Gibbs energy.

1. INTRODUCTION

A number of reports have dealt with the magnetic, electronic, and crystallographic properties of LaMnO_3 (1,2). The magnetic order, moments, and ordering tempera-

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tures of $\text{La}_{1-x}\text{MnO}_{3+\delta}$ depend strongly on the non-stoichiometry (3), and a series on the defect chemistry of $\text{LaMnO}_{3+\delta}$ was reported by Van Roosmalen et al.(4). Although similar physical properties would be expected in other perovskite-structured lanthanoid-manganese-oxides, only a few phase diagram studies that could precisely reveal the non-stoichiometry of LnMnO_3 have been performed (5,6).

Recently, the phase equilibrium has been established in Ln-Mn-O systems at 1100°C (Ln = La (7), Nd (8), Gd (9), Sm (10), Yb and Dy (11), Ho and Tb (12), Eu and Y (13), and Pr and Lu (14)). According to these studies, there are two types of phase diagrams depending on the number of stable ternary compounds in the Ln-Mn-O system, one being the single ternary compound LnMnO_3 and the other two ternary compounds, LnMnO_3 and LnMn_2O_5 . But on account of the stability of Pr_6O_{11} under the present experimental conditions in the Pr-O system, the pattern of the Pr-Mn-O system (14) is different from the latter type with two ternary compounds.

The objectives of the present study are to: (1) establish detailed phase diagrams of the Er-Mn-O and Tm-Mn-O systems at 1100°C as a function of the oxygen partial pressure, (2) know to which types of the phase diagram these established systems belong, (3) determine the thermochemical properties based on the phase equilibrium at 1100°C, and (4) plot ΔG^0 values of the common reaction, $1/2 \text{Ln}_2\text{O}_3 + \text{MnO} + 1/4 \text{O}_2 = \text{LnMnO}_3$, for both systems on the previous line of ΔG^0 vs. tolerance factor.

2. EXPERIMENTAL

Analytical grade Er_2O_3 (99.9%), Tm_2O_3 (99.9%), and MnO (99.9%) were used as starting materials.

The MnO was dried by heating it in air at 110°C, and both of the other oxides were calcined at 1100°C. Mixtures with the desired ratio of Ln_2O_3 to MnO were prepared by mixing thoroughly in an agate mortar and performing repeated calcination during the intermediate mixing. This was followed by the same procedures described previously (15). The thermogravimetric method was used in the present experiment; the oxygen partial pressure was adjusted by passing a gas or mixed gases through the furnace.

The desired oxygen partial pressures were obtained using gas mixtures of CO_2 and H_2 and of CO_2 and O_2 , and the single-component gases O_2 and CO_2 . The apparatus and procedures for controlling the oxygen partial pressure and maintaining a constant temperature, the method of thermogravimetry, and the criterion for the establishment

of equilibrium were the same as described in the previous paper (15). The method for establishing equilibrium can be described briefly as follows. To ensure equilibrium, the equilibrium weight of each sample at a particular oxygen partial pressure was determined from both sides of the reaction; that is, as the oxygen partial pressure was increasing from a lower value and as it was decreasing from a higher value. The balance, furnace, and gas mixer are schematically shown in (16). The furnace was installed vertically, and a mullite tube wound with Pt 60%-Rh 40% alloy wire served as its heating element. Mixed gases, which ensure the desired oxygen partial pressures, passed from the bottom of the furnace to the top. The actual oxygen partial pressures of the gas phase were measured by means of a solid electrolytic cell composed of $(\text{ZrO}_2)_{0.85}(\text{CaO})_{0.15}$ (17).

The identification of phases and the determination of lattice constants were performed using a Rint 2500 Rigaku X-ray diffractometer, with Ni-filtered $\text{CuK}\alpha$ radiation. An external standard silicon was used to calibrate 2θ .

3. RESULTS AND DISCUSSIONS

3-1. Phase equilibrium

3-1-1. Mn-O system

Four oxides, MnO , Mn_3O_4 , Mn_2O_3 , and MnO_2 , have been noted in the Mn-O system. This system was reinvestigated under the present experimental conditions and has been reported in the $\text{La}_2\text{O}_3\text{-MnO-MnO}_2$ system (7). The oxygen partial pressure in equilibrium with MnO and Mn_3O_4 was found to be $\log (P_{\text{O}_2}/\text{atm}) = -5.40 \pm 0.05$ and Mn_3O_4 was stoichiometric over the range of $-\log (P_{\text{O}_2}/\text{atm}) = 0$ to 5.40. MnO , however, is slightly nonstoichiometric, being oxygen-rich with a O/Mn molar ratio of 1.019 at $\log (P_{\text{O}_2}/\text{atm}) = -5.40$. An equation, $N_{\text{O}}/N_{\text{MnO}} = 9.83 \times 10^{-4} (\log P_{\text{O}_2})^2 + 1.914 \times 10^{-2} (\log P_{\text{O}_2}) + 0.0933$, was obtained for the MnO solid solution over the oxygen partial pressure range from -10.00 to -5.40 using the least squares method. Here, we supposed that the MnO solid solution consisted of two components, oxygen and MnO . Therefore, N_{O} and N_{MnO} represent the mole fractions of oxygen and MnO in the solid solution, respectively.

The oxides MnO and Mn_3O_4 were confirmed to be stable, whereas the higher oxides Mn_2O_3 and MnO_2 were not stable. This has also been reported by van Roosmalen et al. in the investigation of the pseudobinary $\text{La}_2\text{O}_3\text{-Mn}_2\text{O}_3$ phase diagram in the atmosphere of air (Fig. 6 in Ref. 18). They showed that below about 1150K, Mn_2O_3 is

stable, but at about 1150~1450K, $t\text{-Mn}_3\text{O}_4$ is stable.

3-1-2. $\text{Er}_2\text{O}_3\text{-MnO-MnO}_2$ system.

Four samples with $\text{Er}_2\text{O}_3/\text{MnO}$ molar ratios of 0.5/0.5, 0.4/0.6, 0.25/0.75, and 0.15/0.85 were prepared for thermogravimetric analysis. The relationships between the oxygen partial pressure, $(-\log(P_{\text{O}_2}/\text{atm}))$, on the ordinate and the ratio of weight changes, $(W_{\text{O}_2}/W_{\text{T}})$, on the abscissa are shown for three representative samples of 0.15/0.85, and 0.4/0.6 in Figs. 1- (a) and (b). Here, W_{O_2} is the weight increase of the samples from the reference weight at $\log(P_{\text{O}_2}/\text{atm}) = -12.00$, at which Er_2O_3 and MnO are stable, and W_{T} is the total weight gain from the reference state to the weight at 1 atm O_2 , at which Er_2O_3 and ErMnO_3 or ErMnO_3 and Mn_3O_4 are stable, depending on the total composition of the samples. As can be seen in the figures, the weight gradually changes with oxygen partial pressure due to the presence of solid solutions. Weight breaks are found at $-\log(P_{\text{O}_2}/\text{atm}) = 7.95$ and 5.40. The value $\log(P_{\text{O}_2}/\text{atm}) = -5.40$, corresponds to the value at

which MnO and Mn_3O_4 are in equilibrium. Table 1 shows the results of phase identification in the Er-Mn-O system. Samples of around 500 mg were prepared for the identification of phases using the quenching method. Four phases, Er_2O_3 , MnO , Mn_3O_4 , and ErMnO_3 were found to be stable.

ErMn_2O_5 , $\text{Er}_2\text{Mn}_2\text{O}_7$, ErMn_2O_4 , Mn_2O_3 and MnO_2 were not stable.

Based on the results of thermogravimetric analysis and phase identification, a phase diagram was constructed for the $\text{Er}_2\text{O}_3\text{-MnO-MnO}_2$ system, even though MnO_2 was not stable under these conditions, as shown in Fig. 2.

The numerical values shown for three of the solid fields in Fig. 2 were the $-\log(P_{\text{O}_2}/\text{atm})$ values at equilibrium,

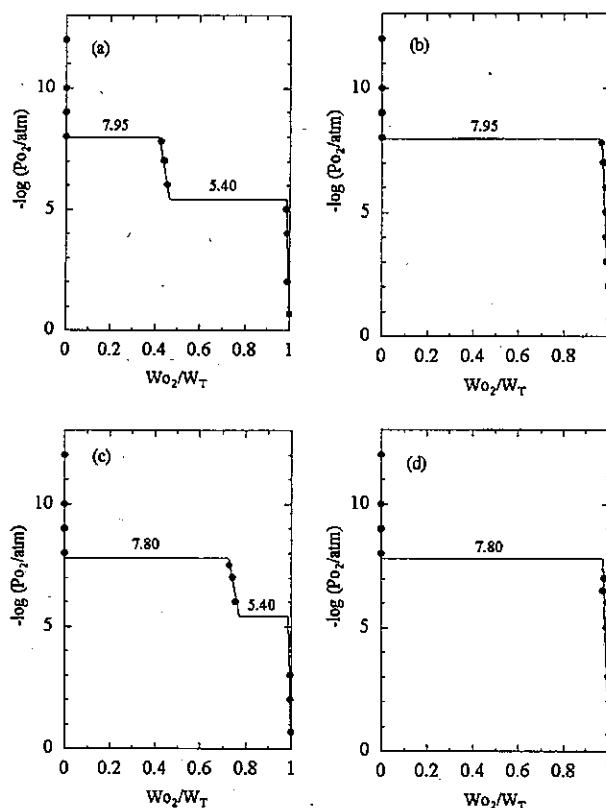


Fig. 1. The relationship between the oxygen partial pressure, $\log(P_{\text{O}_2}/\text{atm})$, and the weight change of the samples, $W_{\text{O}_2}/W_{\text{T}}$: (a) $\text{Er}_2\text{O}_3/\text{MnO} = 0.15/0.85$, (b) $\text{Er}_2\text{O}_3/\text{MnO} = 0.4/0.6$, (c) $\text{Er}_2\text{O}_3/\text{MnO} = 0.25/0.75$, and (d) $\text{Er}_2\text{O}_3/\text{MnO} = 0.50/0.50$.

Table 1. Identification of Phases

Sample		$-\log(P_{O_2}/\text{atm})$	Time/h	Phase		
Er ₂ O ₃	MnO					
0.5	0.5	10.00	23	Er ₂ O ₃ + MnO		
		9.00	24	Er ₂ O ₃ + MnO		
		7.50	24	Er ₂ O ₃ + ErMnO ₃		
		6.00	24	Er ₂ O ₃ + ErMnO ₃		
		0.68	91	Er ₂ O ₃ + ErMnO ₃		
0.25	0.75	10.00	23	Er ₂ O ₃ + MnO		
		9.00	24	Er ₂ O ₃ + MnO		
		7.50	24	ErMnO ₃ + MnO		
		6.00	24	ErMnO ₃ + MnO		
		5.00	24	ErMnO ₃ + Mn ₃ O ₄		
0.15	0.85	10.00	23	Er ₂ O ₃ + MnO		
		9.00	24	Er ₂ O ₃ + MnO		
		7.50	24	ErMnO ₃ + MnO		
		6.00	24	ErMnO ₃ + MnO		
		5.00	24	ErMnO ₃ + Mn ₃ O ₄		
		0.68	91	ErMnO ₃ + Mn ₃ O ₄		
		Tm ₂ O ₃	MnO			
		0.50	0.50	11.00	7	Tm ₂ O ₃ + MnO
				9.00	16	Tm ₂ O ₃ + MnO
				7.50	23	Tm ₂ O ₃ + TmMnO ₃
0.68	45			Tm ₂ O ₃ + TmMnO ₃		
0.20	0.80	11.00	7	Tm ₂ O ₃ + MnO		
		9.00	16	Tm ₂ O ₃ + MnO		
		7.50	23	TmMnO ₃ + MnO		
		6.50	23	TmMnO ₃ + MnO		
		5.00	24	TmMnO ₃ + Mn ₃ O ₄		
		0.68	45	TmMnO ₃ + Mn ₃ O ₄		
		0.10	0.90	1.00	7	Tm ₂ O ₃ + MnO
				9.00	16	Tm ₂ O ₃ + MnO
				7.50	23	TmMnO ₃ + MnO
				6.50	23	TmMnO ₃ + MnO

as indicated. As shown in Fig. 2, there are two three-phase regions, R + A₁ + D₁ and A₂ + P₂ + M, in which the oxygen partial pressures at equilibrium are 7.95 and 5.40 in $-\log(P_{O_2}/\text{atm})$, respectively. It is important to note that there are five two-phase regions, Er₂O₃-MnO, Er₂O₃-ErMnO₃, MnO-ErMnO₃, MnO-Mn₃O₄, and Mn₃O₄-ErMnO₃. ErMnO₃ exhibits non-stoichiometric compositions in the range of $\log P_{O_2} = -7.95$ (P₁) to 0 (P₃), as shown in Fig. 2. A perovskite-structured LaMnO_{3+δ} solid

solution was reportedly to be able to form with excess La as well as with excess Mn by van Roosmalen et al.(18). The same phenomenon does not appear in this three-component system. The relationship between the oxygen partial pressure and the ratio N_{O}/N_{ErMnO_3} is represented by

$$\text{the equation } N_{O}/N_{ErMnO_3} = 2.675 \times$$

$10^{-3} (\log P_{O_2}) - 0.008$. Here, N_{O} and N_{ErMnO_3} show the mole fraction of oxygen and ErMnO₃ in the ErMnO₃ solid solution, respectively.

Table 2 lists the compositions, symbols, oxygen partial pressures in equilibrium, and activities of the components in solid solution applying the same symbols used in Fig. 2. The standard state of the solid solutions was arbitrarily set as $\log a_i = 0$.

Lattice constants of the ErMnO₃ with the hexagonal system are listed in Table 3. A sample having Er₂O₃/MnO ratio of 0.25/0.75 was quenched in air. The phase coexisting with ErMnO₃ is indicated in the last column of Table 3. Present values show a small difference from previous values (19).

3-1-3. Tm₂O₃-MnO-MnO₂ system.

Six samples with Tm_2O_3/MnO molar ratios of 0.6/0.4, 0.5/0.5, 0.3/0.7, 0.25/0.75,

Table 2. Compositions, Symbols, Stability Ranges in Oxygen Partial Pressure, and Activities of Components in Solid Solutions.

Component	Compositions	Symbols	$-\log(P_{O_2}/atm)$	$\log a_i$
MnO	MnO _{1.00}	A	10.00~12.00	0
	MnO _{1.00}	A ₁	7.95	-1.03×10^{-3}
	MnO _{1.00}	A ₂	7.80	-1.00×10^{-3}
	MnO _{1.02}	A ₃	5.40	-1.37×10^{-2}
ErMnO ₃	ErMnO _{2.97}	P ₁	7.95	0
	ErMnO _{2.98}	P ₂	5.40	0.25
	ErMnO _{3.00}	P ₃	0.00	0.074
TmMnO ₃	TmMnO _{2.98}	P ₄	7.55	0
	TmMnO _{2.98}	P ₅	5.40	0.091
	TmMnO _{3.00}	P ₆	0.00	0.054

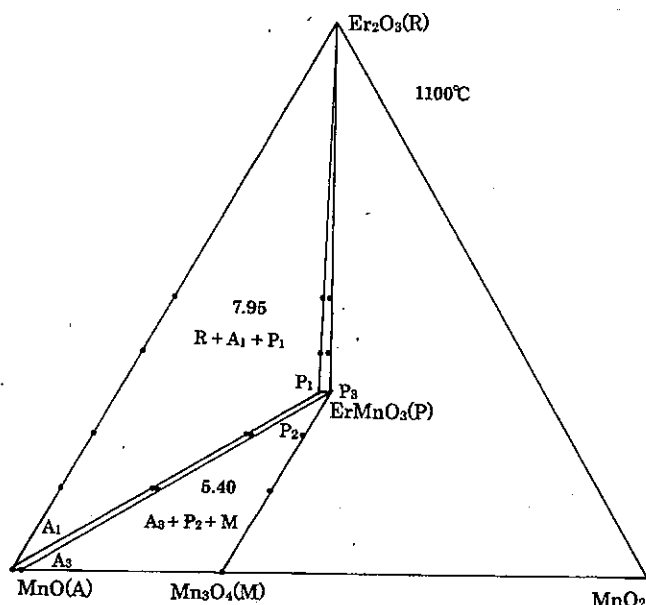


Fig. 2. Phase equilibrium in the $Er_2O_3 \cdot MnO \cdot MnO_2$ system at $1100^\circ C$. Numerical values indicated in the three-solid-phase regions are the oxygen partial pressure in $-\log(P_{O_2}/atm)$ in equilibrium with three solid phases which are shown in the regions. Abbreviations are the same as those in Table 2.

$-\log(P_{O_2}/atm) = 7.80$ and 5.40 . These values correspond to the oxygen partial pressure at which the three-solid phases, $Tm_2O_3(R) + TmMnO_3(P_4) + MnO(A_2)$ and $TmMnO_3(P_5) + MnO(A_3) + Mn_3O_4(M)$ are in equilibrium, respectively. The partial pressure $\log P_{O_2} = -5.40$ corresponds to the equilibrium between MnO and Mn_3O_4 , as described above.

The results of phase identification of the $Tm \cdot Mn \cdot O$ system are shown in Table 1,

0.2/0.8 and 0.1/0.9 were prepared for thermogravimetric analysis. Fig. 1 shows the relationships between the oxygen partial pressure, $-\log(P_{O_2}/atm)$, on the ordinate and the weight change, W_{O_2}/W_T , on the abscissa for two representative samples, 0.5/0.5 (Fig. 1(c)) and 0.1/0.9 (Fig. 1(d)). Here, W_{O_2} is the weight increase of the samples from the reference weight at $\log(P_{O_2}/atm) = -12.00$, at which Tm_2O_3 and MnO are stable, and W_T is the total weight gain from the reference state to the weight at 1 atm O_2 , at which both Tm_2O_3 and $TmMnO_3$, and $TmMnO_3$ and Mn_3O_4 are stable, depending on the total composition of the samples.

Weight breaks are found at

along with those of the $\text{Er}_2\text{O}_3\text{-MnO-MnO}_2$ system. Four phases, Tm_2O_3 , MnO , Mn_3O_4 , and TmMnO_3 , were found to be stable, whereas TmMn_2O_5 , $\text{Tm}_2\text{Mn}_2\text{O}_7$, TmMn_2O_4 , Mn_2O_3 and MnO_2 were not stable in the present experimental setup.

Based on the above thermogravimetric results and phase identifications, a phase diagram was constructed for the $\text{Tm}_2\text{O}_3\text{-MnO-MnO}_2$ system, even though MnO_2 is not stable under the experimental conditions, and this is shown in Fig. 3. The numerical values shown in the three-phase regions of Fig. 3 are the $-\log(\text{P}_{\text{O}_2}/\text{atm})$ values found for the three solid phases, as described above. Abbreviations are the same as those in Table 2. It is important to note that there are five two-

phase regions. TmMnO_3 has a small non-stoichiometric composition in the range of $\log(\text{P}_{\text{O}_2}/\text{atm}) = -7.80$ to 0. Although it is a short range for a solid solution, the relation $\text{No}/\text{N}_{\text{TmMnO}_3}$ vs. the oxygen partial pressure $\log(\text{P}_{\text{O}_2}/\text{atm})$ for the TmMnO_3 solid solution was calculated from the present phase diagram. The following equation was obtained: $\text{No}/\text{N}_{\text{TmMnO}_3} = 2.530 \times 10^{-3} (\log \text{P}_{\text{O}_2}) - 0.005$.

The lattice constants of the hexagonal TmMnO_3 are listed in Table 3, together with the values of ErMnO_3 . A sample with $\text{Tm}_2\text{O}_3/\text{MnO}$ ratios of 0.2/0.8 was quenched in air, $-\log(\text{P}_{\text{O}_2}/\text{atm}) = 0.68$. Phases coexisting with TmMnO_3 are shown in the last column in Table 3. A large difference was found between our lattice constants of TmMnO_3 and previously cited values (20).

Table 3. Lattice constants of Quenched ErMnO_3 and TmMnO_3

Sample	$-\log \text{P}_{\text{O}_2}$ (atm)	a (Å)	c (Å)	V (Å ³)	Coexisted Phase
Er_2O_3 MnO 0.25 0.75	0.68	6.126(4)	11.372(2)	369.6(6)	Mn_3O_4
Ref. 19		6.1166	11.435		
Tm_2O_3 MnO 0.2 0.8	0.68	6.082(4)	11.385(6)	364.8(3)	Mn_3O_4
Ref. 20		6.016	11.376		

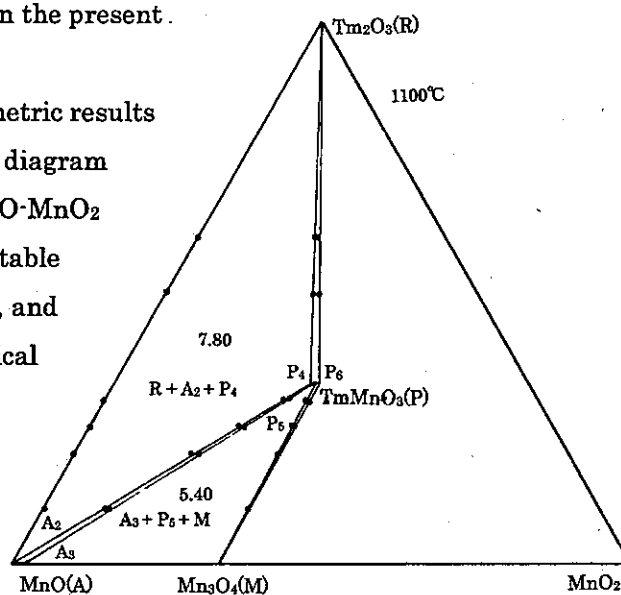


Fig. 3. Phase equilibrium in the $\text{Tm}_2\text{O}_3\text{-MnO-MnO}_2$ system at 1100°C. Numerical values indicated in the three solid phase regions are the oxygen partial pressure in $-\log(\text{P}_{\text{O}_2}/\text{atm})$ in equilibrium with three solid phases which are shown in the regions. Abbreviations are the same as those in Table 2.

3-2. The Standard Gibbs Energy Change of a Reaction

Based on the established phase diagrams, the standard Gibbs energy changes of the reactions corresponding to the phase diagrams were determined from the equation, $\Delta G^\circ = -RT \ln K$, where R is the gas constant, T the absolute temperature, and K the equilibrium constant of the reaction. The results obtained are listed in Table 4. The standard state of the activities of the components in the solid solutions can be arbitrarily chosen for each solid solution as indicated by $\log a_i = 0$ in Table 2. The $-\log (P_{O_2}/\text{atm})$ values and ΔG° columns shown in parentheses in Table 4 are calculated from quoted ΔG° and $\log (P_{O_2}/\text{atm})$ values, respectively.

The standard Gibbs energy change for reaction (1) is -72.1 ± 0.3 kJ/mol. Assuming that the MnO activity of the composition (A_3) is unified, -75.0 ± 0.3 kJ/mol is obtained, as shown in the second line of

Table 4. The standard Gibbs Energy Changes of the Reaction at 1100°C.

Reaction	$-\log P_{O_2}$ (atm)	$-\Delta G^\circ$ (kJ/mol)
(1) $3 \text{ MnO} + 1/2 \text{ O}_2 = \text{Mn}_3\text{O}_4$	5.40	72.1
	5.40	75.0
	(5.62)	73.9 ^a
	(4.60)	60.4 ^b
(2) $1/2 \text{ Er}_2\text{O}_3 + \text{MnO} + 1/4 \text{ O}_2 = \text{ErMnO}_3$	7.95	52.3
	8.01 ^d	(53.7)
(3) $1/2 \text{ Tm}_2\text{O}_3 + \text{MnO} + 1/4 \text{ O}_2 = \text{TmMnO}_3$	7.80	51.3
	7.90	51.9 ^d

Ref. 21: ^b Ref. 22: ^c Ref. 23: ^d Ref. 24:

The values in parentheses are calculated from the quoted ΔG° or the oxygen partial pressures.

Table 4. This difference between the values is due to the small solid solution range. And this value is very similar to the results obtained by Hahn et al.(21). But their other two values are larger by about $10 \sim 20$ kJmol⁻¹ than the present values. The results for reactions (2) and (3) are in good agreement with those obtained by Atsumi et al.(24), even though the experimental methods were different.

3-3. Relationship between tolerance factor and ΔG°

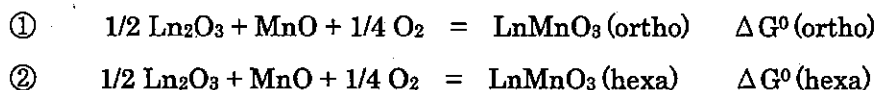
The reaction $1/2 \text{ Ln}_2\text{O}_3 + \text{MnO} + 1/4 \text{ O}_2 = \text{LnMnO}_3$, is common to all of the Ln-Mn-O systems studied so far. The relationship between the ΔG° values of this reaction and the tolerance factor (t) of perovskite structures with 12-coordinated lanthanoid atoms is shown in Fig. 4. Previously reported values (7, 8, 9, 10, 11, 12) of ΔG° are also shown in Fig. 4 for comparison. The solid circles represent values for orthorhombic system, and open circles represent values for hexagonal systems. Ionic radii given by Espinosa (25) were used to calculate the tolerance factors. The ionic

radii for Er and Tm are 1.276 Å and 1.271 Å from 12-coordinated garnet, respectively, and the ionic radius of O^{2-} was taken to be 1.40 Å. The crystal structures of $ErMnO_3$ and $TmMnO_3$ are hexagonal. Thus, it may be problematic to adapt tolerance factors based upon the orthorhombic perovskite structure to both hexagonal oxides. As can be seen in Fig. 4, the Gibbs energy change of the reaction was nearly proportional to the tolerance factor for a perovskite structure. The values of Er and Tm are well fitted

to the equation, $\Delta G^0(\text{hexa}) = -5.885 \times 10^2 t + 4.908 \times 10^2$ that was presented by Kitayama et al.(12). This is shown by a dotted line, and $\Delta G^0(\text{ortho})$ vs. tolerance factor (t) is shown by a solid line in Fig. 4.

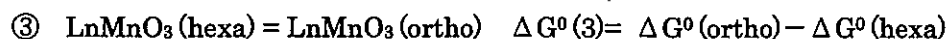
3-4. The Gibbs energy change of the phase transition

So far, in the series of the Ln-Mn-O system, the reaction, $1/2 Ln_2O_3 + MnO + 1/4 O_2 = LnMnO_3$, has been found to be common. We have obtained two such reactions, namely:



Here, $LnMnO_3(\text{ortho})$ and $LnMnO_3(\text{hexa})$ and $\Delta G^0(\text{ortho})$ and $\Delta G^0(\text{hexa})$ denote the manganite of orthorhombic and hexagonal crystal $LnMnO_3$ and the Gibbs energy changes of reactions ① and ②, respectively.

Deducting equation ② from ①, we find equation ③:



This equation shows the transition from the hexagonal to the orthorhombic system.

Here, $\Delta G^0(3)$ is the Gibbs energy change of reaction (3), that is, the Gibbs energy change of the transition from the hexagonal to the orthorhombic system.

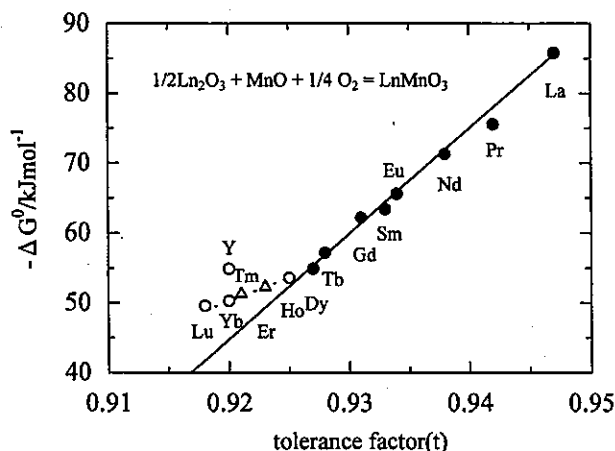


Fig. 4

Fig. 4. The relationship between the ΔG^0 value of the reaction, $1/2 Ln_2O_3 + MnO + 1/4 O_2 = LnMnO_3$, and the tolerance factor (t). Solid circles indicate previous values for orthorhombic systems, and open circles represent previous values for hexagonal systems. The open triangles are the present values of $ErMnO_3$ and $TmMnO_3$. These values are well-fitted to the hexagonal line.

Assuming that the ΔG^0 (ortho) of ErMnO_3 and TmMnO_3 can be extrapolated by the equation, ΔG^0 (ortho) = $-1.518 \times 10^3 t + 1.352 \times 10^3$ (from La to Tb), we can obtain ΔG^0 (3) for the above manganites by calculation. The results are tabulated in Table 5.

Table 5 Estimated ΔG^0 (trans)/kJmol⁻¹ values for ErMnO_3 and TmMnO_3

LnMnO ₃	t	- ΔG^0 (hexa)	- ΔG^0 (ortho)*	ΔG^0 (trans)
ErMnO ₃	0.923	52.3	49.1	3.2
TmMnO ₃	0.921	51.3	46.1	5.2

* Extrapolated values calculated from the general equation for orthorhombic LnMnO₃.

The ΔG^0 (trans) values for ErMnO_3 and TmMnO_3 are 3.2 and 5.2 kJmol⁻¹, respectively. So, these reactions do not take place in the hexagonal to orthorhombic direction at 1100°C. This means that physical energy (for example $P \Delta V$) is needed in order for the reaction ③ to take place from left to right. That is, if a volume change (ΔV) were to be found, from the hexagonal system to the orthorhombic system of ErMnO_3 and TmMnO_3 , the pressure (P) could be estimated and ascertained by a high pressure apparatus.

4. Conclusion

- 1) Phase equilibria in the system Ln-Mn-O (Ln = Er and Tm) at 1100°C were established under an oxygen partial pressure ranging from 0 to -12.00 in log(P_{O_2} /atm).
- 2) Under the present experimental conditions, the Ln_2O_3 , MnO, Mn_3O_4 , and LnMnO_3 phases are stable in both systems.
- 3) MnO, ErMnO_3 , and TmMnO_3 have non-stoichiometric composition. However, Mn_3O_4 is stoichiometric. The ranges of non-stoichiometry for both ErMnO_3 and TmMnO_3 are very small.
- 4) The lattice constants of quenched ErMnO_3 , and of TmMnO_3 were determined and compared with previous values. The values we obtained are not in agreement with the previous values.
- 5) The standard Gibbs energies of the reactions found in the diagram were calculated with the oxygen partial pressure in equilibrium with three solid phases.
- 6) ΔG^0 values for the reaction, $1/2 \text{Ln}_2\text{O}_3 + \text{MnO} + 1/4 \text{O}_2 = \text{LnMnO}_3$, for hexagonal ErMnO_3 and TmMnO_3 , fit the linear equation of the tolerance factor (t) vs. ΔG^0

$$\Delta G^0$$
 (hexa) = $-6.426 \times 10^2 t + 5.406 \times 10^2$.
- 7) The Gibbs energy changes of the transition, ErMnO_3 (hexa) = ErMnO_3 (ortho) and

TmMnO₃ (hexa) and TmMnO₃ (ortho), were determined as 3.2 and 5.2 kJmol⁻¹, under assumption that the ΔG^0 (ortho) value equation for ErMnO₃ and TmMnO₃ was applicable.

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